RV4141A
Low Power Ground Fault Interrupter

Features

- Powered from the AC line
- Built-in rectifier
- Direct interface to SCR
- 500 µA quiescent current
- Precision sense amplifier
- Adjustable time delay
- Minimum external components
- Meets UL 943 requirements
- For use with 110V or 220V systems
- Available in an 8-pin SOIC package

Description

The RV4141A is a low-power controller for AC receptacle ground fault circuit interrupters. These devices detect hazardous current paths to ground and ground to neutral faults. The circuit interrupter then disconnects the load from the line before a harmful or lethal shock occurs.
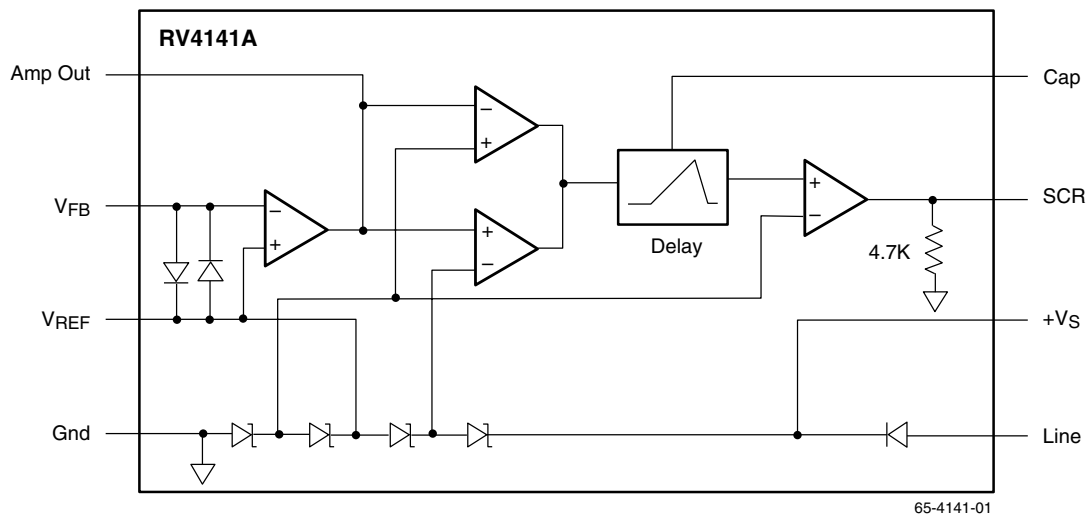
Internally, the RV4141A contains a diode rectifier, shunt regulator, precision sense amplifier, current reference, time delay circuit, and SCR driver.

Two sense transformers, SCR, solenoid, three resistors and four capacitors complete the design of the basic circuit interrupter. The simple layout and minimum component count ensure ease of application and long term reliability.
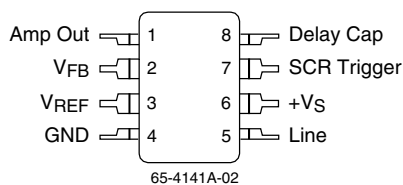
Features not found in other GFCI controllers include a low offset voltage sense amplifier eliminating the need for a coupling capacitor between the sense transformer and sense amplifier, and an internal rectifier to eliminate high voltage rectifying diodes.

The RV4141A is powered only during the positive half period of the line voltage, but can sense current faults independent of its phase relative to the line voltage. The gate of the SCR is driven only during the positive half cycle of the line voltage.

Block Diagram

65-4141-01

Pin Assignments

Amp Out	1	8	Delay Cap
V_{FB}	2	7	SCR Trigger
V_{REF}	3	6	$+V_S$
GND	4	5	Line

65-4141A-02

Absolute Maximum Ratings

(beyond which the device may be damaged)[1]

Parameter		Min	Typ	Max	Units
Supply Current				10	mA
Internal Power Dissipation				500	mW
Storage Temperature Range		-65		+150	°C
Operating Temperature Range		-35		+80	°C
Junction Temperature				125	°C
Lead Soldering Temperature	10 Sec, SOIC			260	°C

Notes:

1. Functional operation under any of these conditions is NOT implied. Performance and reliability are guaranteed only if the Electrical Characteristics are not exceeded.

Thermal Characteristics

Parameter			Min	Typ	Max	Units
θ_{JA}	Thermal resistance	SOIC		240		°C/W

Electrical Characteristics $(I_{LINE} = 1.5mA$ and $T_A = +25°C$, $R_{SET} = 650k\Omega)$

Parameters	Test Conditions	Min	Typ	Max	Units
Shunt Regulator (Pins 5 to 4)					
Regulated Voltage	$I_{2-3} = 11\mu A$	25.0	27.0	29.0	V
Regulated Voltage	$I_{LINE} = 750\ \mu A$, $I_{2-3} = 9\mu A$	25.0	27.0	29.0	V
Quiescent Current	$V_{5-4} = 24V$	—	500	—	µA
Sense Amplifier (Pins 2 to 3)					
Offset Voltage		-200	0	200	µV
Gain Bandwidth	(Design Value)	—	3	—	MHz
Slew Rate	(Design Value)		1.0		V/µS
Input Bias Current	(Design Value)		30	100	nA
SCR Trigger (Pins 7 to 4)					
Output Resistance	$V_{7-4} = $ Open, $I_{2-3} = \mu A$	3.8	4.7	5.6	kΩ
Output Voltage	$I_{2-3} = 9\mu A$	0	0.1	10	mV
Output Voltage	$I_{2-3} = 11\mu A$	3.0	3.8	4.5	V
Output Current	$V_{7-4} = 0V$, $I_{2-3} = 11\mu A$	400	600		µA
Reference Voltage (Pins 3 to 4)					
Reference Voltage	$I_{LINE} = 750\ \mu A$	12.0	13.0	14.0	V
Delay Timer (Pins 8 to 4)					
Discharge/Charge ratio	$I_{2-3} = 0/11\mu A$	1.8	2.5	3.0	µA/µA
Delay Time (Note 1)	$C_{8-4} = 12nF$	—	2.0	—	ms
Delay Current	$I_{2-3} = 11\mu A$	30	40	50	µA

Note:

1. Delay time is defined as starting when the instantaneous sense current (I_{2-3}) exceeds $6.5\ V/R_{SET}$ and ending when the SCR trigger voltage V_{7-6} goes high.

Circuit Operation

(Refer to Block Diagram and Figure 1)

The precision op amp connected to Pins 1 through 3 senses the fault current flowing in the secondary of the sense transformer, converting it to a voltage at Pin 1. The ratio of secondary current to output voltage is directly proportional to feedback resistor, R_{SET}.

R_{SET} converts the sense transformer secondary current to a voltage at Pin 1. Due to the virtual ground created at the sense amplifier input by its negative feedback loop, the sense transformer's burden is equal to the value of R_{IN}. From the transformer's point of view, the ideal value for R_{IN} is 0Ω. This will cause it to operate as a true current transformer with minimal error. However, making R_{IN} equal to zero creates a large offset voltage at Pin 1 due to the sense amplifier's very high DC gain. R_{IN} should be selected as high as possible consistent with preserving the transformer's operation as a true current mode transformer. A typical value for R_{IN} is between 200 and 1000Ω.

As seen by the equation below, maximizing R_{IN} minimizes the DC offset error at the sense amplifiers output. The DC offset voltage at Pin 1 contributes directly to the trip current error. The offset voltage at Pin 1 is:

$$V_{OS} \times R_{SET}/(R_{IN} + R_{SEC})$$

Where:
V_{OS} = Input offset voltage of sense amplifier
R_{SET} = Feedback resistor
R_{IN} = Input resistor
R_{SEC} = Transformer secondary winding resistance

The sense amplifier has a specified maximum offset voltage of 200 μV to minimize trip current errors.

Two comparators connected to the sense amplifier output are configured as a window detector, whose references are -6.5V and +6.5V, referred to Pin 3. When the sense transformer secondary RMS current exceeds $4.6/R_{SET}$ the output of the window detector starts the delay circuit. If the secondary current exceeds the predetermined trip current for longer than the delay time a current pulse appears at Pin 7, triggering the SCR.

The SCR anode is directly connected to a solenoid or relay coil. The SCR can be tripped only when its anode is more positive than its cathode.

Supply Current Requirements

The RV4141A is powered directly from the line through a series limiting resistor called R_{LINE}, its value is between 24 kΩ and 91 kΩ. The controller IC has a built-in diode rectifier eliminating the need for external power diodes.

The recommended value for R_{LINE} is 24 kΩ to 47 kΩ for 110V systems and 47 kΩ to 91 kΩ for 220V systems. When R_{LINE} is 47 kΩ the shunt regulator current is limited to 3.6 mA. The recommended maximum peak line current through R_{LINE} is 10 mA.

GFCI Application (Refer to Figure 1)

The GFCI detects a ground fault by sensing a difference current in the line and neutral wires. The difference current is assumed to be a fault current creating a potentially hazardous path from line to ground. Since the line and neutral wires pass through the center of the sense transformer, only the differential primary current is transferred to the secondary. Assuming the turns ratio is 1:1000 the secondary current is 1/1000th the fault current. The RV4141A's sense amplifier converts the secondary current to a voltage which is compared with either of the two window detector reference voltages. If the fault current exceeds the design value for the duration of the programmed time delay, the RV4141A will send a current pulse to the gate of the SCR.

Detecting ground to neutral faults is more difficult. R_B represents a normal ground fault resistance, R_N is the wire resistance of the electrical circuit between load/ neutral and earth ground. R_G represents the ground to neutral fault condition. According to UL 943, the GFCI must trip when $R_N = 0.4\Omega$, $R_G = 1.6\Omega$ and the normal ground fault is 6 mA.

Assuming the ground fault to be 5 mA, 1 mA and 4 mA will go through R_G and R_N, respectively, causing an effective 1 mA fault current. This current is detected by the sense transformer and amplified by the sense amplifier. The ground/ neutral and sense transformers are now mutually coupled by R_G, R_N and the neutral wire ground loop, producing a positive feedback loop around the sense amplifier. The newly created feedback loop causes the sense amplifier to oscillate at a frequency determined by ground/neutral transformer secondary inductance and C4. Typically it occurs at 8 KHz.

C2 is used to program the time required for the fault to be present before the SCR is triggered. Refer to the equation below for calculating the value of C2. Its typical value is 12 nF for a 2 ms delay.

R_{SET} is used to set the fault current at which the GFCI trips. When used with a 1:1000 sense transformer, its typical value is 1 MΩ for a GFCI designed to trip at 5 mA.

R_{IN} should be the highest value possible which ensures a predictable secondary current from the sense transformer. If R_{IN} is set too high, normal production variations in the transformer permeability will cause unit to unit variations in the secondary current. If it is too low, a large offset voltage error at Pin 1 will be present. This error voltage in turn creates a trip current error proportional to the input offset voltage of the sense amplifier. As an example, if R_{IN} is 500Ω,

R$_{SET}$ is 1 MΩ, R$_{SEC}$ is 45Ω and the V$_{OS}$ of the sense amplifier is its maximum of 200 μV, the trip current error is ±5.6%.

The SCR anode is directly connected to a solenoid or relay coil. It can be tripped only when its anode is more positive than its cathode. It must have a high dV/dt rating to ensure that line noise (generated by electrically noisy appliances) does not falsely trigger it. Also the SCR must have a gate drive requirement less than 200 μA. C3 is a noise filter that prevents high frequency line pulses from triggering the SCR.

The relay solenoid used should have a response time of 3 ms or less to meet the UL 943 timing requirement.

Sense Transformers and Cores

The sense and ground/neutral transformer cores are usually fabricated using high permeability laminated steel rings. Their single turn primary is created by passing the line and neutral wires through the center of its core. The secondary is usually from 200 to 1500 turns.

Transformers may be obtained form Magnetic Metals, Inc. (www.magmet.com)

Calculating the Values of R$_{SET}$ and C2

Determine the nominal ground fault trip current requirement. This will be typically 5 mA in North America (117V AC) and 22 mA in the UK and Europe (220V AC). Determine the

minimum delay time required to prevent nuisance tripping. This will typically be 1 to 2 ms. The value of C2 required to provide the desired delay time is:

$$C2 = 6 \times T$$

where:
C2 is in nF
T is the desired delay time in ms.

The value of R$_{SET}$ to meet the nominal ground fault trip current specification is:

$$R_{SET} = \frac{4.6 \times N}{I_{FAULT} \times COS\ 180(T/P)}$$

where:
R$_{SET}$ is in kΩ
T is the time delay in ms
P is the period of the line frequency in ms
I$_{FAULT}$ is the desired ground fault trip current in mA RMS
N is the number of sense transformer secondary turns.

This formula assumes an ideal sense transformer is used. The calculated value of R$_{SET}$ may have to be changed up to 30% to when using a non-ideal transformer.


Note:
1. Portions of this schematic are subject to U.S. patents 3,878,435 and Re. 30,678.
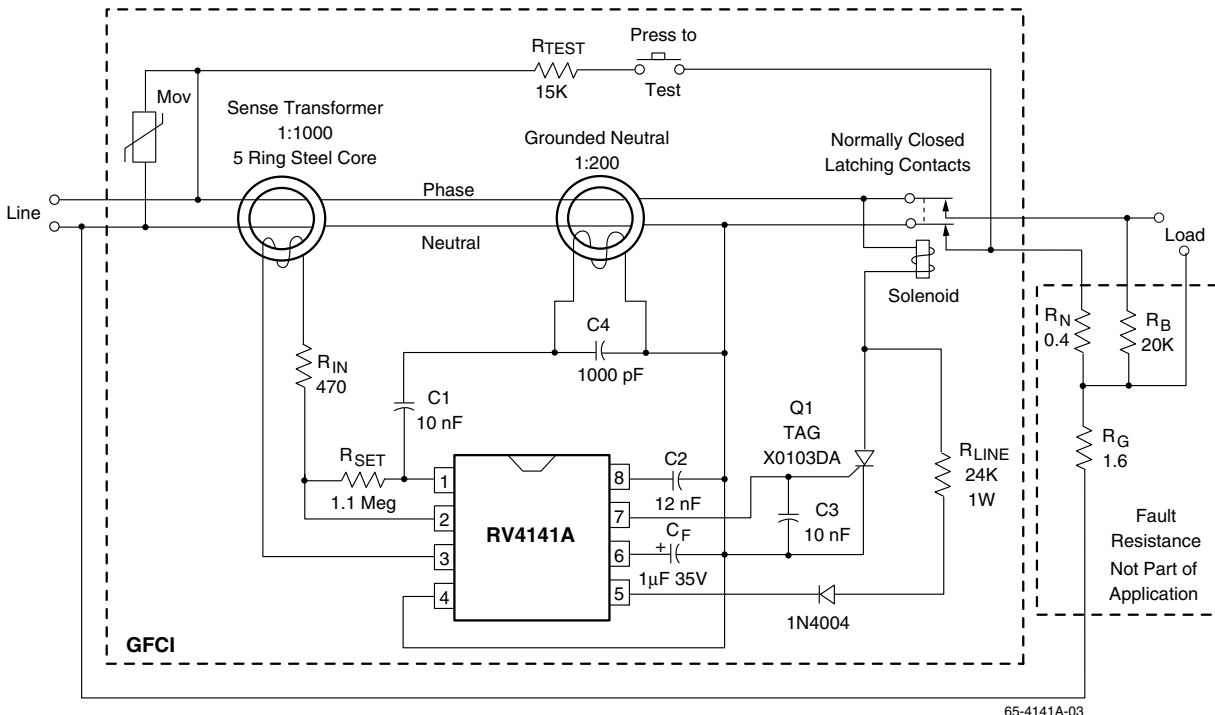
Figure 1. GFI Application Circuit

Mechanical Dimensions

8-Lead SOIC Package

Symbol	Inches		Millimeters		Notes
	Min.	Max.	Min.	Max.	
A	.053	.069	1.35	1.75	
A1	.004	.010	0.10	0.25	
B	.013	.020	0.33	0.51	
C	.008	.010	0.20	0.25	5
D	.189	.197	4.80	5.00	2
E	.150	.158	3.81	4.01	2
e	.050 BSC		1.27 BSC		
H	.228	.244	5.79	6.20	
h	.010	.020	0.25	0.50	
L	.016	.050	0.40	1.27	3
N	8		8		6
α	0°	8°	0°	8°	
ccc	—	.004	—	0.10	

Notes:

1. Dimensioning and tolerancing per ANSI Y14.5M-1982.
2. "D" and "E" do not include mold flash. Mold flash or protrusions shall not exceed .010 inch (0.25mm).
3. "L" is the length of terminal for soldering to a substrate.
4. Terminal numbers are shown for reference only.
5. "C" dimension does not include solder finish thickness.
6. Symbol "N" is the maximum number of terminals.
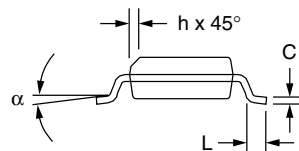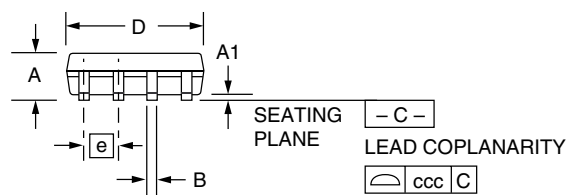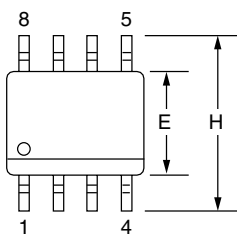
Ordering Information

Part Number	Package	Pb-Free	Operating Temperature Range	Packing Method
RV4141AMT	8-lead Plastic SOIC	No	-35°C to +80°C	Tape and Reel

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